# IMU error calibration of strapdown inertial navigation system 

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#### Abstract

In view of the accuracy of strapdown inertial navigation system to the turntable, the difficulty of installation leveling and North alignment, as well as the various factors such as temperature rise, temperature change of hardware circuit board and components for a long time, the IMU is proposed to take the reference north angle, roll angle and pitch angle of the three-axis turntable as the reference, the actual movement speed of the system as the observation measurement, and the minimum is adopted Two multiplication fitting system level calibration algorithm, through three axis turntable multi-position static measurement, rotation angle measurement, rapid measurement of 24 parameters such as installation error and orthogonal error of inertial unit, sensor zero deviation, scale factor, etc., the system level calibration time is not more than 2 h , and the course and attitude progress is better than $0.012^{\circ}$. This method is not only convenient and simple, but also convenient to improve the system accuracy and rapid batch production.


Keywords: IMU; Zero Bias; Installation Error; Least Square Method; Three Axis Turntable;

## 1. INTRODUCTION

The IMU of laser gyro strapdown inertial navigation system is composed of three laser gyroscopes and three accelerometers. Its non orthogonal installation, sensor bias, scale factor and other errors directly affect the accuracy of the system. Therefore, IMU error calibration is a very important link in the development and use of strapdown inertial navigation system. At home and abroad, discrete calibration method and system level calibration method are often used. The discrete calibration method needs to provide the attitude reference [1] through the precise test equipment, take the earth's rotation speed, gravity acceleration and rotation platform angular speed as the reference quantity, and compare with the actual output of gyroscope and accelerometer, so as to solve various error coefficients, but when the laser gyroscope works, it will produce jitter itself, thus affecting the calibration accuracy. The system level calibration method mainly uses the output of the inertial instrument to solve the navigation problem, and takes the navigation error as the observation measurement to determine the error parameters, avoiding the use of the precision instrument, but its calculation is large, the filtering algorithm is complex, and the calibration time is long [2].

In view of the shortcomings of the above two methods, as well as the difficulty of the turntable in the process of calibration to the north and to adjust equally [3], this paper proposes a system level multi position 24 parameter calibration method, which can identify all the parameters through the rotating position of the manual or automatic three-axis turntable, and the whole calibration process takes about 2 hours. This method takes velocity as the observation measurement, uses the least square method to calibrate 24 parameters, such as the orthogonal installation of three-axis laser gyro and accelerometer, sensor bias, scale factor, etc. its algorithm is simple and efficient, and improves the accuracy of the system IMU.

## 2. IMU ERROR MODEL BUILDING

There are errors in the mechanical installation of the three laser gyroscopes and three accelerometers of the main components of the laser gyro strapdown inertial navigation system. The laser gyro coordinate system and the accelerometer sensor itself cannot be completely orthogonal in the engineering installation, and there is a certain deflection angle [4]. The two
coordinate systems of laser gyroscope and accelerometer can not overlap completely, and they are also non orthogonal error sources. In addition, the output value of the angular velocity of the laser gyro fixed on the turntable rotating $360^{\circ}$ is inconsistent with the theoretical value, and the output value of the accelerometer in the positive and negative directions is inconsistent with the corresponding value of the theoretical value, so the calibration factor needs to be calibrated; at the same time, the output value of the sensor in the zero position has errors. The system level calibration with the least square fitting method is adopted. Through the three-axis turntable with multiple positions: static rotation static [5], the laser gyro strapdown inertial navigation system remains static in the fixed position. After the initial heading is given and the calibration preparation is completed, it rotates or rotates to the designated position according to the pre-designed direction. After the system remains static, the data of the system is measured. The test time is $t$, and through observation The change of the system speed and the change of the sensor in the process of rotation are measured, 24 error parameters are calibrated, and a total of 14 steps are carried out.

In the calibration process, the northeast sky coordinate system is defined as the reference coordinate system [4], and the error equation of laser gyro is:
$\left\{\begin{array}{l}\omega_{1 x}=b_{11} \omega_{x}+b_{12} \omega_{y}+b_{13} \omega_{z}-B_{01} \\ \omega_{1 y}=b_{21} \omega_{x}+b_{22} \omega_{y}+b_{23} \omega_{z}-B_{02} \\ \omega_{1 z}=b_{31} \omega_{x}+b_{32} \omega_{y}+b_{33} \omega_{z}-B_{03}\end{array}\right.$
Formula: $\omega_{1 x} \omega_{1 y}, \omega_{1 z}$ is the output angular velocity of the laser gyro after the calibration parameters are brought in; $B_{01}, ~ B_{02}, ~ B_{03}$ is the laser gyro bias; $b_{11}, b_{22}, ~ b_{33}$ is the laser gyro scale factor, also known as the scale factor, $b_{12}, ~ b_{13}, ~ b_{21}, ~ b_{23}, ~ b_{31}, b_{32}$ is the installation error of the laser gyro.

The error equation of accelerometer is:
$\left\{\begin{array}{l}a_{t x}=a_{11} a_{x}+a_{12} a_{y}+a_{13} a_{z}-A_{01} \\ a_{t y}=a_{21} a_{x}+a_{22} a_{y}+a_{23} a_{z}-A_{02} \\ a_{t z}=a_{31} a_{x}+a_{32} a_{y}+a_{33} a_{z}-A_{03}\end{array}\right.$
Formula: A1 is the speed increment of the accelerometer output after the calibration parameters are brought in; A2 is the accelerometer bias; A3 is the accelerometer scale factor, also known as the accelerometer scale factor; A4 is the accelerometer installation error.

## 3. IMU calibration scheme design

After the inertial components of the laser gyro strapdown inertial navigation system are installed in the fixed box structure, due to various errors, three laser gyro and three accelerometers have certain error angles with the northeast of the theoretical coordinate system. The system is fixed on the calibrated three-axis turntable, and the installation error of laser gyro and acceleration and turntable error are controlled within 3 '. The error between the actual position of IMU and the theoretical value of navigation coordinate system is shown in Figure 1. Definition of IMU and navigation coordinate system: $E_{l} N_{l} U_{l}$ is the actual position of the inertial combination of laser gyro strapdown navigation system; ENU is the navigation coordinate system of northeast sky, and there is a certain deviation angle between them. The system is fixed on the manual three-axis turntable as shown in Figure 2.


Figure 1. Comparison between IMU component installation and theoretical coordinate system


Figure 2. The system is fixed on the manual three-axis turntable
The IMU speed error is:

$$
\begin{align*}
\delta \dot{V}^{n}= & -\phi^{n} \times f^{n}-\left(-2 \omega_{i e}^{n}+\omega_{e n}^{n}\right) \times \delta V^{n}  \tag{3}\\
& -\left(2 \delta \omega_{i e}^{n}+\omega_{e n}^{n}\right) \times V^{n}+C_{b}^{c} \delta f^{b}
\end{align*}
$$

During the calibration process, the system does not displace, so, $V^{n}=0, \omega_{e n}^{n}=0$ 。

The rotation velocity of the earth is very small compared with that of the turntable , $-2 \omega_{i e}^{n} \times \delta V^{n}$ ignored, So the velocity error equation is:
$\delta \dot{V}^{n}=-\phi^{n} \times f^{n}$
Before IMU calibration, the fixed system shall be installed, and the initial position of the turntable shall be aligned with the north direction, that is, the turntable shall be fixed at 0 degrees position, and the system heading, roll and pitch shall be aligned with 0 degrees. Pre installed 24 calibration parameters, the scale factor of x axis, y axis, z axis laser gyro is 0.932920 , the scale factor of x axis, y axis, z axis accelerometer is 1.0 , and the initial value of other parameters is 0 . The data acquisition period $\tau=5 \mathrm{~ms}$, that is, $\tau=0.005 \mathrm{~s}$ for three laser gyroscopes and three accelerometers. When each position is stationary, the data acquisition period is 100 s , that is, the acquisition number $\mathrm{n}=20000, \Delta V_{e 1}$ and $\Delta V_{e 2}$ are the eastward velocity at T1 and T2, and the constant $\mathrm{K}=180 / \pi$. The steps of IMU calibration are as follows:

1) Calibrate the scale factors $a_{11}, a_{22}$ and $a_{33}$ of the accelerometer, and zero bias $A_{01}, A_{02}$ and $A_{03}$. First, fix the system, rotate the three-axis turntable to the position of heading 0 degrees, roll 0 degrees, pitch 0 degrees, and keep the system still. Given the heading 0 degrees, collect the data for 100 s after the north seeking is completed. Then, slowly and uniformly rotate 90 degrees along the pitch direction, i.e., rotate the pitch from 0 degrees to 90 degrees, keep the static collection data for 100s. then rotate -180 degrees in the pitch direction, rotate to -90 degrees, collect the data for 100 s . Then rotate 90 degrees in the pitch direction to 0 degrees , rotate 90 degrees in the roll direction to 90 degrees, and collect data for 100 s ; rotate 180 degrees in the roll direction, that is, rotate the roll from 90 degrees to -90 degrees, collect data for 100 s ; finally return to the initial position. The position of the system on the three-axis turntable is shown in Figure 3 to figure 7 in turn, and finally returns to figure 3. The heading, roll and pitch are respectively represented by $\mathrm{H}, \mathrm{R}$ and P .


Figure 3. $H=0^{\circ} \mathbf{R}=\mathbf{0}^{\circ} \mathbf{P}=\mathbf{0}^{\circ}$


Figure 4. $\mathrm{H}=\mathbf{0}^{\circ} \mathrm{R}=\mathbf{0}^{\circ} \mathrm{P}=+90^{\circ}$


Figure 5. $\mathrm{H}=0^{\circ} \mathrm{R}=\mathbf{0}^{\circ} \mathrm{P}=-90^{\circ}$


Figure 6. $\quad \mathrm{H}=\mathbf{0}^{\circ} \mathrm{R}=+90^{\circ} \mathrm{P}=\mathbf{0}^{\circ}$


Figure 7. $H=0^{\circ} \mathbf{R}=0^{\circ} \mathbf{P}=-90^{\circ}$

The bias parameter and accelerometer scale factor are as follows:

$$
\begin{aligned}
& \left\{\begin{array}{l}
A_{01}+=\left(\sum_{i=1}^{20000} a_{x_{-} p(i)}+\sum_{i=1}^{20000} a_{x_{-} m(i)}\right) / T_{100} / 2 \\
A_{02}+=\left(\sum_{i=1}^{20000} a_{y_{-} p(i)}^{20000}+\sum_{i=1}^{200} a_{y_{-} m(i)}\right) / T_{100} / 2 \\
A_{03}+=\left(\sum_{i=1}^{20000} a_{z_{-} p(i)}+\sum_{i=1}^{2000} a_{z_{-} m(i)}\right) / T_{100} / 2
\end{array}\right. \\
& \left\{\begin{array}{l}
a_{11}=a_{11} /\left(\left(\sum_{i=1}^{20000} a_{x_{-} p(i)}-\sum_{i=1}^{20000} a_{x_{-} m(i)}\right) / T_{100} / 2\right) \\
a_{22}=a_{22} /\left(\left(\sum_{i=1}^{20000} a_{y_{-} p(i)}-\sum_{i=1}^{20000} a_{y_{-} m(i)}\right) / T_{100} / 2\right) \quad(6) \\
a_{33}=a_{33} /\left(\left(\sum_{i=1}^{20000} a_{z_{-} p(i)}-\sum_{i=1}^{20000} a_{z_{-} m(i)}\right) / T_{100} / 2\right)
\end{array}\right.
\end{aligned}
$$

Formula: $a_{x_{-} p}, a_{y_{-} p}$ and $a_{z_{-} p}$ are the corresponding accelerometer 90 degrees position measurement values; $a_{x_{-} m}, a_{y_{-} m}$ and $a_{z_{-} m}$ are the corresponding accelerometer -90 degrees position measurement values; the sensor data acquisition cycle of laser gyro strapdown inertial navigation system is 5 ms , and the data measurement time of each position is $\mathrm{T}_{100}$ equals 100 s .
2) Calibrate the scale factor $n_{11}$ of the x -axis laser gyro. The system rotates to the position of heading 0 degrees, roll 0 degrees, pitch 0 degrees and remains still (see Figure 3); then the given heading is 0 degrees, after initialization, the system rotates slowly and uniformly 360 degrees along the pitch direction and collects data for 100s; then it rotates slowly and uniformly -360 degrees along the pitch direction, i.e. returns to the starting position and collects data for 100s.

$$
n_{11}=n_{11}\left(1.0-\left(\left(\Delta V_{e 1}-\Delta V_{e 2}\right) / 2\right) /\left(2 \pi \times g \times T_{100} \times \tau\right)\right.
$$

3) Calibrate the scale factor $n_{33}$ of z-axis laser gyro. The system rotates to the position of heading - 90 degrees, roll 0 degrees, pitch 0 degrees, and remains stationary, as shown in Figure 8. When the given heading is -90 degrees and initialization is completed, the data shall be collected for 100 seconds by slowly and uniformly rotating 360 degrees along the pitch direction; then the data shall be collected for 100s by slowly and uniformly rotating -360 degree along the pitch direction, and then returned to the initial position.


Figure8. $\quad \mathbf{H}=-90^{\circ} \mathbf{R}=0^{\circ} \mathbf{P}=0^{\circ}$
$n_{33}=n_{33}\left(1.0-\left(\left(\Delta V_{e 1}-\Delta V_{e 2}\right) / 2\right) /\left(2 \pi \times g \times T_{100} \times \tau\right)\right.$
4) Calibrate the scale factor $n_{22}$ of $y$-axis laser gyro. The system rotates to the position of heading -90 degrees, roll -90 degrees, pitch 0 degrees and remains stationary, i.e. from the initial position (see Figure 8) to the calibration preparation position (see Figure 9). The given heading is -90 degrees, after initialization, the data will be collected for 100 s by slowly and uniformly rotating 360 degrees along the pitch direction, and then slowly and uniformly rotating -360 degrees along the pitch direction, and the data will be collected for 100 s , and then return to the initial position.


Figure9. $\mathrm{H}=-90^{\circ} \mathrm{R}=-90^{\circ} \mathrm{P}=\mathbf{0}^{\circ}$
$n_{22}=n_{22}\left(1.0-\left(\left(\Delta V_{e 1}-\Delta V_{e 2}\right) / 2\right) /\left(2 \pi \times g \times T_{100} \times \tau\right)(9)\right.$
5) Calibrate the zero deviation $A_{03}$ of $z$-axis accelerometer. The system rotates to the position of heading 0 degrees, roll 0 degrees, pitch 0 degrees, and remains still. Then the heading 0 degrees is given. After initialization, the system slowly and uniformly rotates 180 degrees along the roll direction and collects data for 100s; then it slowly and uniformly rotates -180 degrees along the roll direction and returns to the initial position and collects data for 100s; then it continues to slowly and uniformly rotate -180 degrees along the roll direction and collects data for 100 s . Then slowly and uniformly rotate 180 degrees along the rolling direction to return to the initial position.
$A_{03}-=\left[\left(\Delta V_{e 1}+\Delta V_{e 2}\right) / 2\right] /\left(2 \times g \times T_{100}\right)$
6) Calibrate the zero deviation $A_{01}$ of $x$-axis accelerometer. The system rotates to the position of heading - 90 degrees, roll 0 degrees, pitch 0 degrees, and remains still. Given the heading 90 degrees, after initialization, the system slowly and uniformly rotates 180 degrees along the pitch direction and collects data for 100s; then it slowly and uniformly rotates - 180 degrees along the pitch direction and returns to the initial position and collects data for 100 s ; then it continues to slowly and uniformly rotate -180 degrees along the pitch direction and collects
data for 100s; then it rolls along the roll direction Slowly and uniformly rotate 180 degrees to return to the initial position.

$$
\begin{equation*}
A_{01}+=\left[\left(\Delta V_{e 1}+\Delta V_{e 2}\right) / 2\right] /\left(2 \times g \times T_{100}\right) \tag{11}
\end{equation*}
$$

7) Calibrate the zero deviation $A_{02}$ of $y$-axis accelerometer and the installation error $a_{23}$ of $y$ axis accelerometer and z -axis accelerometer. The system rotates to the position of heading 0 degrees, roll 0 degrees, pitch 0 degrees and remains still. Then the heading 0 degrees is given. After initialization, the system slowly and uniformly rotates 90 degrees along the roll direction and collects data for 100s. Then it slowly and uniformly rotates -90 degrees along the roll direction and returns to the initial position and collects data for 100 s . Then it continues to slowly and uniformly rotate -90 degrees along the roll direction and collects data for 100s. Finally, slowly and uniformly rotate 90 degrees along the rolling direction to return to the initial position.

$$
\begin{align*}
& A_{02}+=\left[\left(\Delta V_{e 1}-\Delta V_{e 2}\right) / 2\right] /\left(2 \times g \times T_{100}\right)  \tag{12}\\
& a_{23}+=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)
\end{align*}
$$

8) Calibrate the installation error $a_{12}$ of $x$-axis accelerometer and $y$-axis accelerometer. The system rotates to the position of heading -90 degrees, roll 0 degrees, pitch 0 degrees, and remains still. Then the given heading - 90 degrees is given. After initialization, the system slowly and uniformly rotates 90 degrees along the pitch direction and collects data for 100s; then slowly and uniformly rotates -90 degrees along the pitch direction and returns to the initial position and collects data for 100s. Then continue to slowly and uniformly rotate -90 degrees along the pitch direction to collect data for 100s; then slowly and uniformly rotate 90 degrees along the pitch direction to return to the initial position.
$a_{12}-=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)(14)$
9) Calibrate the installation error of $x$-axis accelerometer and $z$-axis accelerometer $a_{13}$. The system rotates to the position of heading -90 degrees, roll -90 degrees and pitch 0 degrees to keep still, and then gives the heading -90 degrees. After initialization, the system slowly and uniformly rotates 90 degrees along the pitch direction (around the $y$-axis), and collects data for 100 s ; then slowly and uniformly rotates -90 degrees along the pitch direction, and returns to the initial position to collect data for 100 s . Then continue to slowly and uniformly rotate -90 degrees along the pitch direction to collect data for 100s; finally, slowly and uniformly rotate 90 degrees along the pitch direction to return to the initial position.
$a_{13}-=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)(15)$
10) The installation errors of y -axis laser gyro and x -axis laser gyro are $n_{21}$ and $n_{31}$ respectively. The system rotates to the position of heading -90 degrees, roll 0 degrees, pitch 0 degrees, and remains still. Then the given heading is -90 degrees. After initialization, the system slowly and uniformly rotates 90 degrees along the roll direction and collects data for 100s; then it slowly and uniformly rotates -90 degrees along the roll direction and returns to the initial position and collects data for 100 s; then it continues to slowly and uniformly rotate 90 degrees along the roll direction and collects data for 100s. Finally, slowly and uniformly rotate 90 degrees along the rolling direction to return to the initial position.
$n_{21}-=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)(16) n_{31}-=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)$
11) The installation errors of the x -axis laser gyro and the y -axis laser gyro are $n_{12}$ and $n_{32}$ respectively. The system rotates to the position of heading -90 degrees, roll 0 degrees, pitch 0 degrees, and remains still, then gives the heading -90 degrees. After initialization, it slowly and uniformly rotates 90 degrees along the heading direction and collects data for 100 s ; then it slowly and uniformly rotates -90 degrees along the heading direction and returns to the initial position and collects data for 100 s; then it continues to slowly and uniformly rotate -90 degrees along the heading direction and collects data for 100s. Finally, slowly and uniformly rotate 90 degrees along the heading direction to return to the initial position.
$n_{32}+=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)$
$n_{12}+=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)$
12) The installation errors of $y$-axis laser gyro and $z$-axis laser gyro are calibrated to be $n_{23}$, and that of x -axis laser gyro and z -axis laser gyro to be $n_{13}$. The system rotates to the position of heading 0 degrees, roll 0 degrees, pitch 0 degrees, and remains still, and then sets the heading 0 degrees. After initialization, the system slowly and uniformly rotates 90 degrees along the pitch direction and collects data for 100s; then slowly and uniformly rotates -90 degrees along the pitch direction and returns to the initial position and collects data for 100s; then continues to slowly and uniformly rotate -90 degrees along the pitch direction and collects data for 100s. Finally, slowly and uniformly rotate 90 degrees along the pitch direction to return to the initial position.
$n_{23}+=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)$
$n_{13}+=\left(\left(\Delta V_{e 1}+\Delta V_{e 2}\right) /\left(2 \times g \times T_{100}\right)\right)$
13) Calibrate the bias $\mathrm{N}_{01}$ of x -axis laser gyro, $\mathrm{N}_{02}$ of y -axis laser gyro and $\mathrm{N}_{03}$ of z -axis laser gyro. The system rotates to the position of heading 0 degrees, roll 0 degrees and pitch 0 degrees to keep still, and then gives the heading 0 degrees. After initialization, keep still to collect data for 600 s, and the system automatically calculates the zero deviation $\mathrm{N}_{01}, \mathrm{~N}_{02}$ and $\mathrm{N}_{03}$ of the X -, Y - and z -axis laser gyro as follows:
$N_{01}+=3600 \times K \times V_{e} / 2 \mathrm{R}(22)$
$N_{02}-=3600 \times K \times \psi / T_{10}$
$N_{03}-=3600 \times K \times V_{n} / 2 R(24)$
Formula: R is the long half axis of the earth; $\mathrm{V}_{\mathrm{e}}$ is the East speed; $\mathrm{V}_{\mathrm{N}}$ is the North speed; T 10 $=600 \mathrm{~s}$.
14) Calibrate the bias $\mathrm{N}_{02}$ and $\mathrm{N}_{03}$ of y -axis and z-axis laser gyro. The system rotates to the position of heading - 90 degrees, roll 0 degrees, pitch 0 degrees and keeps still, then gives the heading -90 degrees, and after initialization, keeps still to collect data for 600 s. based on the thirteen steps, the system automatically calculates the zero deviation $\mathrm{N}_{02}$ and $\mathrm{N}_{03}$ of Y -axis and z-axis laser gyro as follows:

$$
\begin{align*}
& N_{02}-=3600 \times K \times\left((\psi-i k 0 / K) / T_{10}\right)  \tag{25}\\
& N_{03}+=3600 \times K \times V_{e} / 2 R
\end{align*}
$$

Formula: $\psi$ is the heading at the time of data acquisition; $\mathrm{ik} 0=-90^{\circ}$ is the given initial heading.

## 4. IMU error calibration and application of strapdown inertial navigation system

IMU of strapdown inertial navigation system adopts three-axis laser gyro and three-axis quartz accelerometer components, and its system accuracy is verified by using high-precision three-axis digital display turntable to verify the attitude repeatability and orthogonality.

### 4.1 IMU error calibration of strapdown inertial navigation system

The IMU of strapdown inertial navigation system is installed and fixed on the three-axis turntable. The IMU heading is fixed according to the turntable's heading. After the initialization of the system's starting heading is completed, 24 parameters are calibrated
according to the above 14 steps, and parameter files are automatically generated and written into the configuration files. Each time the system opens 24 configuration files are automatically read and loaded into the corresponding parameters. See Table 1 for details.

Table 1. Comparison between initial value of IMU calibration and calibration completion parameters

| number | Calibration parameter | variable | Calibration results |
| :---: | :---: | :---: | :---: |
| 1 | Zero deviation of x -axis laser gyro $(\% / \mathrm{h})$ | $\mathrm{N}_{01}$ | -0.078921 |
| 2 | Zero deviation of y-axis laser gyro ( $\%$ h ) | $\mathrm{N}_{02}$ | +0.025013 |
| 3 | Zero deviation of z-axis laser gyro | $\mathrm{N}_{03}$ | +0.084675 |
| 4 | Zero deviation of x -axis accelerometer(g) | $\mathrm{A}_{01}$ | +0.003576 |
| 5 | Zero deviation of y -axis accelerometer(g) | $\mathrm{A}_{02}$ | -0.0016021 |
| 6 | Zero deviation of z -axis accelerometer(g) | $\mathrm{A}_{03}$ | -0.0059875 |
| 7 | X-axis laser gyro scale factor | $\mathrm{n}_{11}$ | +0.932978 |
| 8 | X-axis laser gyro installation error | $\mathrm{n}_{12}$ | +0.001801 |
| 9 | X -axis laser gyro installation error | $\mathrm{n}_{13}$ | -0.000801 |
| 10 | Y-axis laser gyro installation error | $\mathrm{n}_{21}$ | -0.001657 |
| 11 | Y-axis laser gyro scale factor | $\mathrm{n}_{22}$ | +0.932801 |
| 12 | Y-axis laser gyro installation error | $\mathrm{n}_{23}$ | +0.000914 |
| 13 | Z-axis laser gyro installation error | $\mathrm{n}_{31}$ | +0.000510 |
| 14 | Z-axis laser gyro installation error | $\mathrm{n}_{32}$ | -0.004321 |
| 15 | Z-axis laser gyro scale factor | $\mathrm{n}_{3}$ | +0.932801 |
| 16 | X-axis accelerometer scale factor | $\mathrm{a}_{11}$ | +0.980101 |
| 17 | X -axis accelerometer installation error | $\mathrm{a}_{12}$ | $+0.000801$ |
| 18 | X -axis accelerometer installation error | $\mathrm{a}_{13}$ | -0.000330 |
| 19 | Y-axis accelerometer installation error | $\mathrm{a}_{21}$ | $+0.000000$ |
| 20 | Y-axis accelerometer scale factor | $\mathrm{a}_{22}$ | +1.080798 |
| 21 | Y-axis accelerometer installation error | $\mathrm{a}_{23}$ | +0.000986 |
| 22 | Z-axis accelerometer installation error | $\mathrm{a}_{31}$ | +0.000000 |
| 23 | Z-axis accelerometer installation error | $\mathrm{a}_{32}$ | +0.000000 |
| 24 | Z-axis accelerometer scale factor | $\mathrm{a}_{33}$ | +0.953105 |

Note: except the marked calibration parameters have units, the rest are dimensionless.

### 4.2 IMU accuracy verification of strapdown inertial navigation system

The error of the three-axis high-precision digital display turntable is better than 0.0001 degrees, Level the high-precision digital display turntable, fix the IMU on the turntable [6], prepare for the corresponding test, turn on the power to seek the North twice and take the average value, set it as the initial value of the scale of the three-axis high-precision digital display turntable, and automatically seek the north four times for each quadrant, as shown in table 2-5.

Table 2. test data of $\mathbf{0}^{\circ}, \mathbf{9 0}^{\circ}, 180^{\circ}$ and $270^{\circ}$ position of turntable. unit: ${ }^{\circ}$

| numb |  | $0^{\circ}$ |  |  | $90^{\circ}$ |  |  | $180^{\circ}$ |  |  | $270^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $e r$ | Head | Roll | Pitch | Head | Roll | Pitch | Head | Roll | Pitch | Head | Roll | Pitch |
| 1 | 0.0103 | 0.002 |  | 90.009 | 0.0026 | 0.000 | 180.00 | 0.0019 | 0.002 | 270.00 | 0.003 | 0.002 |
|  | 29 | 115 | $641$ | 189 | 78 | 563 | 0315 | 52 | 138 | 5671 | 548 | 896 |
| 2 | - 0.0106 | 0.002 | - 0.001 | 90.007 | 0.0020 | 0.000 | 180.00 | 0.0016 | 0.003 | 270.00 | 0.003 | 0.002 |
|  | 53 | 893 | $273$ | 654 | 18 | 781 | 0363 | 31 | 159 | 5751 | 179 | 765 |
| 3 |  | 0.003 |  | 89.999 | 0.0026 | 0.000 | 180.00 | 0.0021 | 0.001 | 270.00 | 0.003 | 0.002 |
|  | $72$ | 542 | $101$ | 781 | 71 | 603 | 0403 | 52 | 876 | 6012 | 019 | 514 |
| 4 | 0.0023 | 0.003 | 0.001 | 90.003 | 0.0030 | 0.000 | 180.00 | 0.0019 | 0.002 | 270.00 | 0.003 | 0.003 |
|  | 89 | 679 | $978$ | 2167 | 189 | 451 | 0158 | 871 | 819 | 5138 | 998 | 065 |
| avera <br> ge <br> value | 0.0009 | 0.003 | 0.001 | 90.004 | 0.0025 | 0.000 | 180.00 | 0.0019 | 0.002 | 270.00 | 0.003 | 0.002 |
|  | $02$ |  | $75$ | 96 | 96 | 6 | 03 | 31 | 498 | 56 | 436 | 81 |
| Mean |  |  |  |  |  |  |  |  |  |  |  |  |
| squar | 0.0092 | 0.000 | 0.000 | 0.0042 | 0.0004 | 0.000 | 0.0001 | 0.0002 | 0.000 | 0.0003 | 0.000 | 0.000 |
| deviat | 159 | 716 | 372 | 82 | 18 | 137 | 07 | 18 | 593 | 67 | 435 | 232 |
| ion |  |  |  |  |  |  |  |  |  |  |  |  |

### 4.3 Verify the stability of IMU of strapdown navigation system

The IMU of laser gyro strapdown inertial navigation system is fixed on the chassis of the vehicle body [7], and the central axis of the vehicle body is roughly consistent with the central axis of the vehicle body. The experimental vehicle is equipped with a high-precision azimuth extraction device and a digital level, without accumulated error. The accuracy of the azimuth
extraction device is higher than 0.006 degrees, the course stability is verified; the accuracy of the digital level is better than 0.0006 degrees. After the initialization of IMU, the binding initial heading value of azimuth extraction device and the binding roll and pitch value of digital level are consistent with the initial value of IMU equipment. The closed-loop sports car test results in a certain place are shown in Table 3.

Table 3. test data of $270{ }^{\circ}$ position of turntable. unit: ${ }^{\circ}$

| number | IMU |  |  | Azimuth lead | Digital level |  | error |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Head | Roll | Pitch | Head | Roll | Pitch | Head | Roll | Pitch |
| 1 | 20.186751 | 0.009256 | $0.017475$ | 20.186751 | 0.009256 | $0.017475$ | 0.000000 | 0.000000 | 0.000000 |
| 2 | 74.261759 | 0.017019 | 0.052811 | 74.262023 | 0.017211 | 0.052833 | $0.000264$ | $0.000192$ | $0.000022$ |
| 3 | 156.123621 | 0.009978 | 0.039101 | 156.124101 | 0.009981 | 0.039131 | $0.000480$ | $0.000003$ | $0.000030$ |
| 4 | 254.556781 | 0.019298 | 0.029012 | 254.557014 | 0.019301 | 0.029112 | $0.000233$ | $0.000003$ | $0.000100$ |
| 5 | 246.017871 | 0.008066 | $0.027013$ | 246.018541 | 0.008054 | $0.027128$ | $0.000670$ | 0.000012 | 0.000115 |
| 6 | 20.017897 | 0.012601 | $0.013012$ | 20.017913 | 0.012871 | $0.014151$ | $0.000016$ | $0.000270$ | 0.001139 |

From the test data in Table 3, it can be seen that the heading stability is better than 0.009 degrees and the roll and pitch accuracy is better than 0.06 degrees.

## 5. Concluding remarks

In this paper, the IMU error calibration method based on the laser gyro strapdown inertial navigation system is proposed, which solves the difficulties of the system calibration due to the accuracy of the turntable, the alignment of the base to the north and the leveling, the dithering of the laser gyro, the rise of the working temperature for a long time and the complexity of the algorithm. The system level calibration method based on the IMU output speed is proposed Through multi position measurement of three-axis turntable: static rotation static, 24 error parameters such as orthogonal installation error of three-axis laser gyro and three-axis accelerometer, zero deviation of sensor and scale factor are identified quickly. The calibration process is shortened to 2 hours, and the attitude accuracy is better than 0.012 degrees. The
experiment shows that the algorithm is simple and the operation process is convenient. It can effectively solve the influence of turntable error on IMU calibration accuracy, thus improving the accuracy of laser gyro strapdown inertial navigation system and providing reference value for IMU error calibration.

## Acknowledgements

Research project of Chongqing Higher Education Teaching Reform (No.: 183263), general research project of Chongqing higher education teaching reform "information teaching research and practice based on blue ink cloud class in management course" (No.: 183263), research project of Chongqing higher education teaching reform "exploration of performance management course Ideological and political teaching reform" (No.: 193472),intelligent navigation innovation team of Chongqing Youth Vocational and Technical College (No.: cqy2018td05)

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